

An aerial photograph of a tidal estuary, showing a network of water channels and land areas. The water is a deep blue, and the land is a mix of green and brown. A semi-transparent blue rectangular box is overlaid on the top half of the image, containing the title text. The text is in a bold, orange-red font and is underlined.

Trapping of sediment in tidal estuaries

Henk Schuttelaars
Delft Institute of Applied Mathematics,
TU Delft

Introduction (1)

Estuary: semi-enclosed body of water where salt and fresh water meet.

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Chesapeake Bay: Length: 315 km
Width: 5-56 km
Av. depth: 8.5 m

German Wadden Sea:



Introduction (2)

Many estuaries exhibit an **E**stuarine **T**urbidity **M**aximum comprising fine, suspended muddy sediments.



1. Potomac
2. Chesapeake Bay
3. Delaware
4. Severn



Introduction (3)

Other example: Ems estuary.



Ems River at a glance

$\sim 12,600 \text{ km}^2$

$Q_{\text{avg}} \sim 70 \text{ m}^3/\text{s}$

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Our focus: Ems
Estuary

Shipping most
Important Industry

e.g. MeyerWerft

Large Implications for river
And estuarine dynamics!

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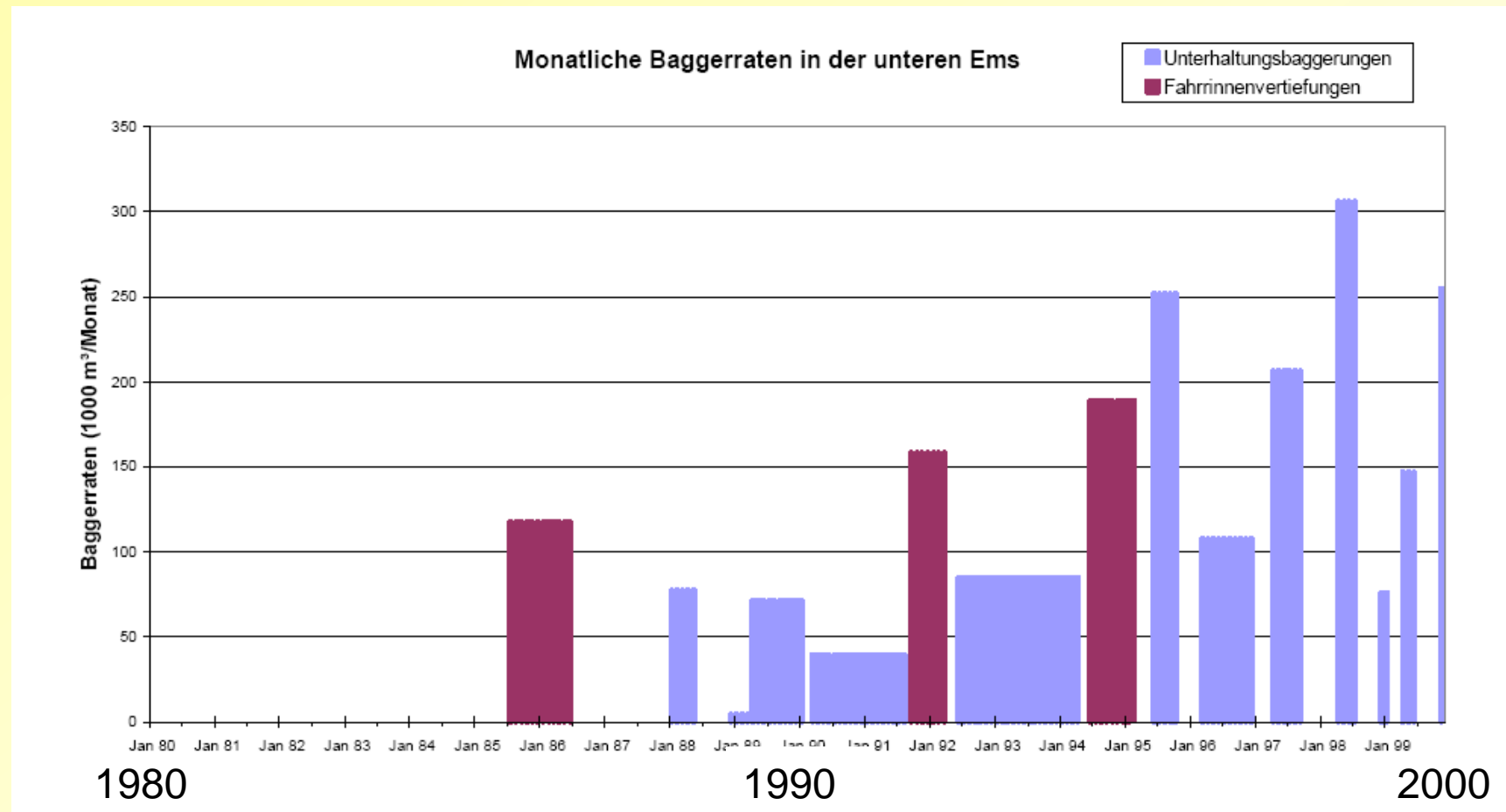
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Large Implications for river
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Introduction (4)

Increase in Dredging



Monthly dredging rates in the Ems between Emden and Pappenburg between 1980 and 2000, in units of 1000 m³/month. Adapted from Habermann, 2003.

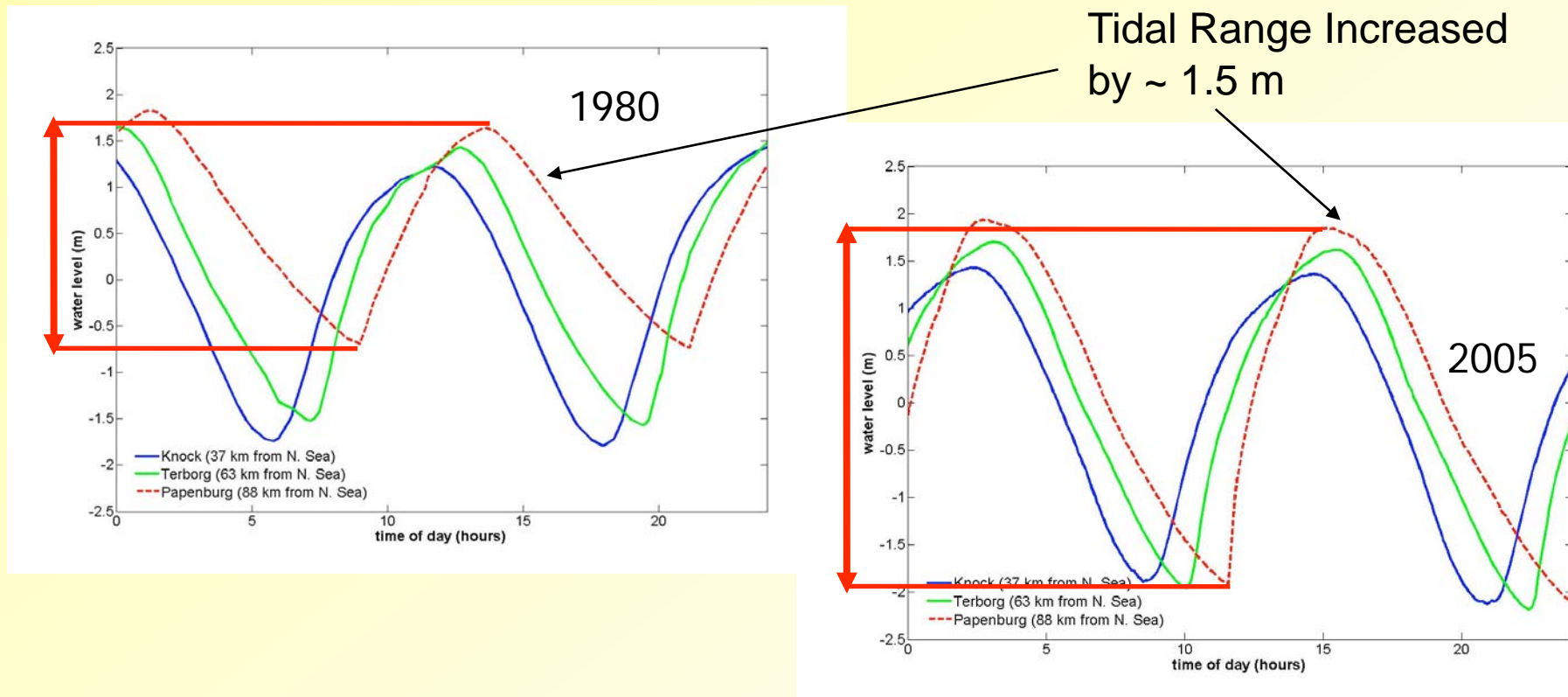
Introduction (5)

This resulting in

1. a significant change in tidal motion (safety)

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Changes in horizontal velocity?

Introduction (5)

This resulting in

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2. a significant increase of turbidity (environment)

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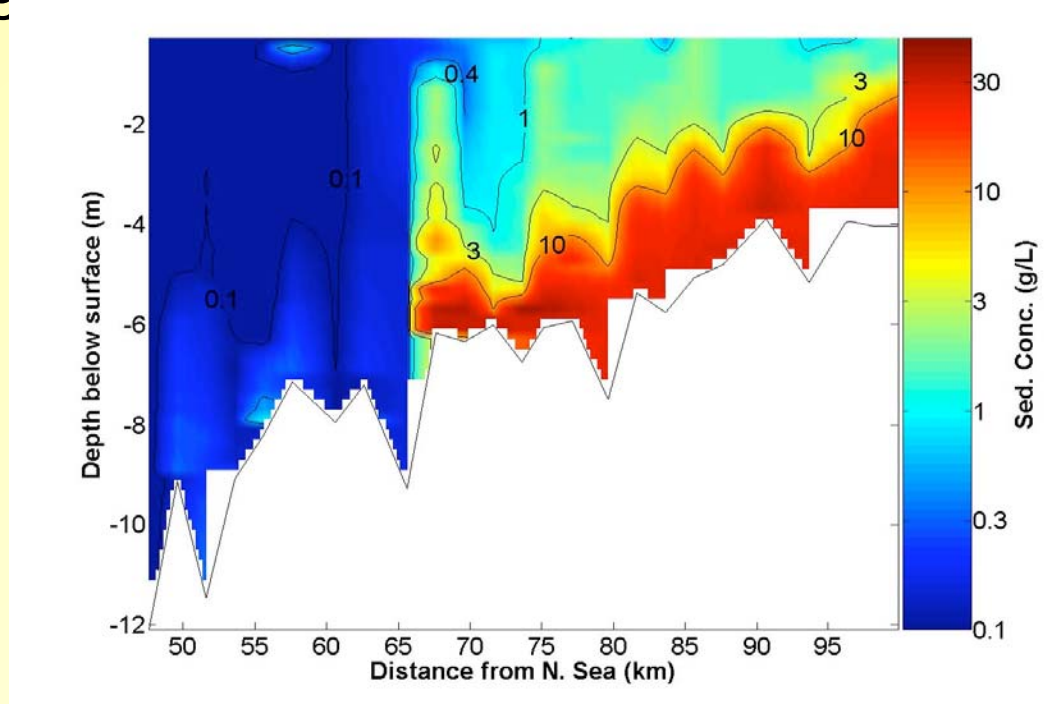
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Introduction (6)

This resulting in

1. a significant change in tidal motion (safety)
2. a significant increase of turbidity (environment)



- Turbidity maximum has moved upstream;
- High turbidity zone now extended into the freshwater zone to Papenburg;

Research Questions

- Can the observed changes in the water motion be modelled and understood?
- Which mechanisms result in trapping of sediment in the Ems and what has changed over the years?

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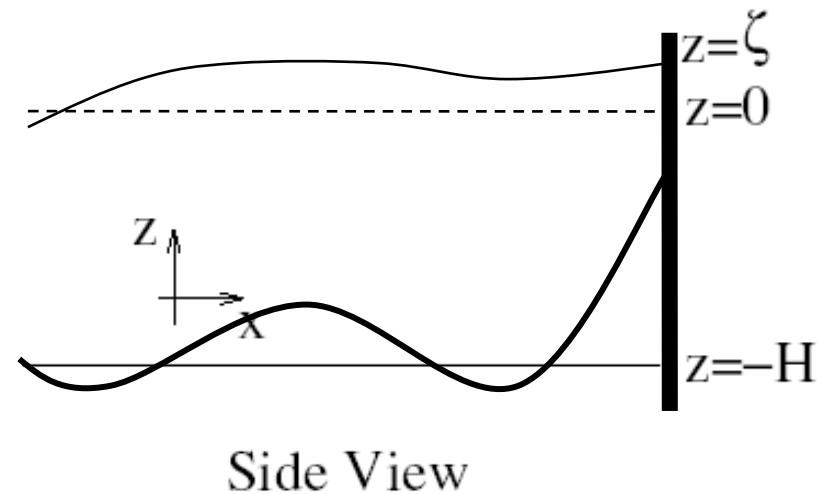
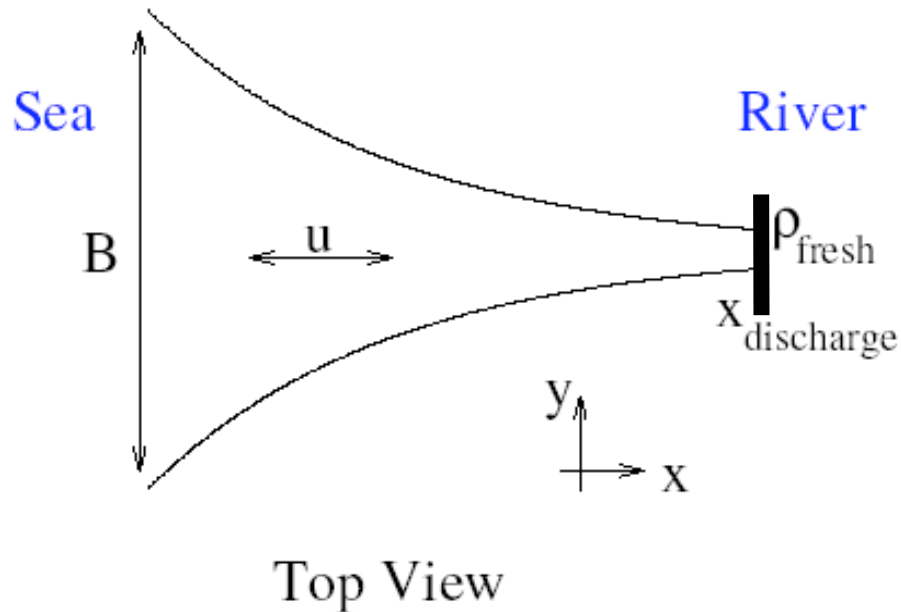
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Main Results

Essential ingredients

- Decrease of bed friction and vertical mixing and a deepening of the channel
- Along-estuary varying erosion coefficient (~ layer of fine sediment)
- Temporal settling lag effects + external overtides

Model Formulation (1)



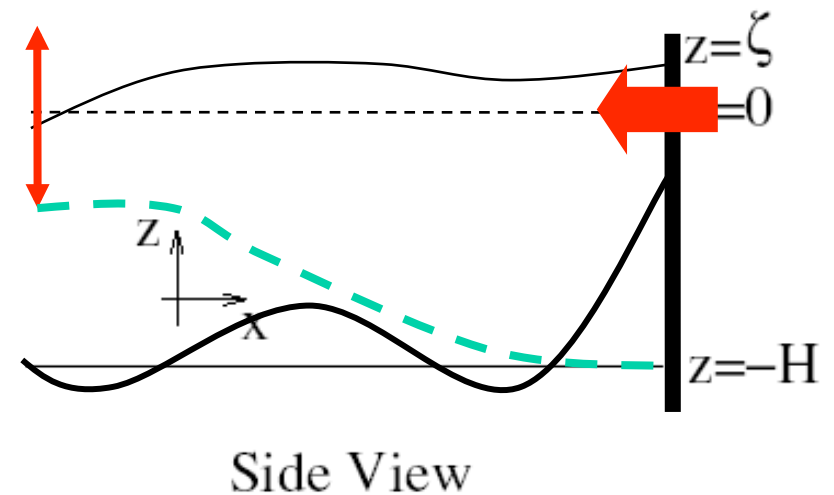
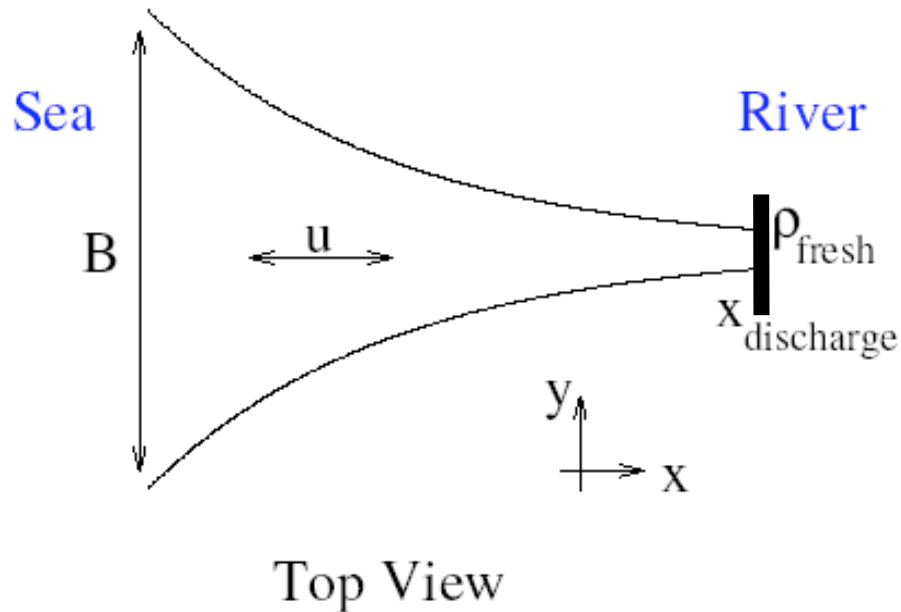
Geometry:

- weakly convergent
- prescribed (fixed) bed

Forcing:

- sea side: M_2 and M_4 water elevation
- river side: fresh water flux
- prescribed density gradient

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$$u_x + w_z - \frac{u}{L_b} = 0,$$
$$u_t + uu_x + wu_z + g\zeta_x - \frac{g\rho_x}{\rho_0}(z - \zeta) - (A_v u_z)_z = 0.$$

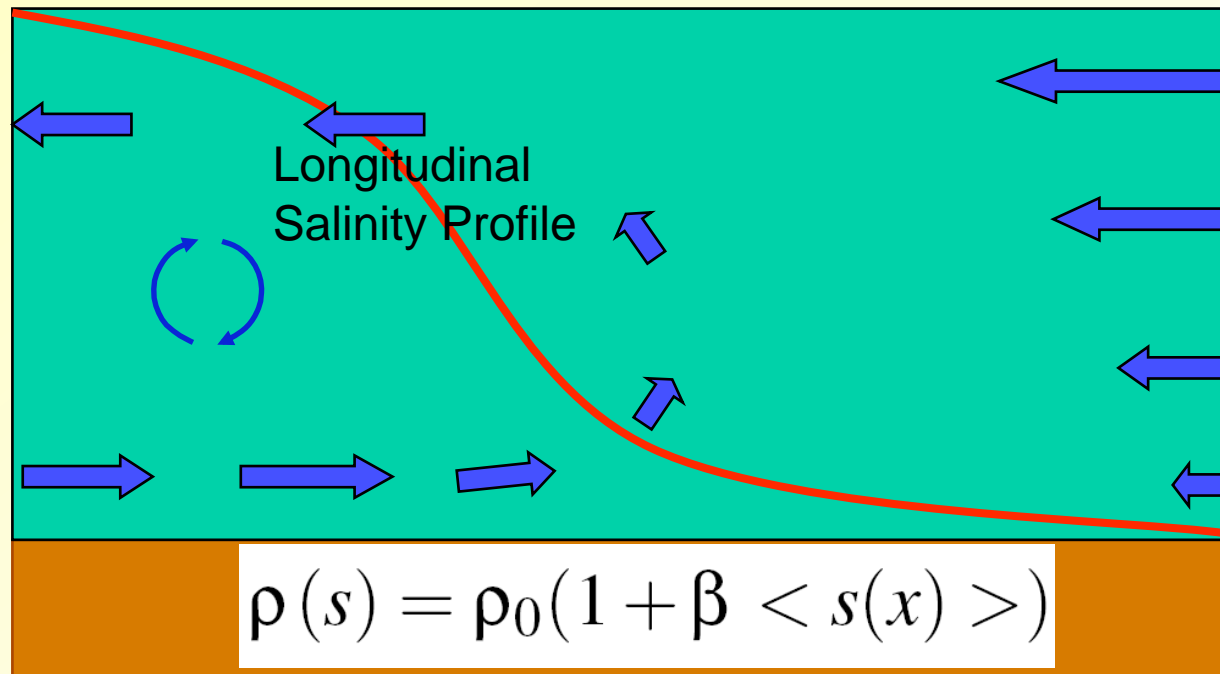
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boundary conditions

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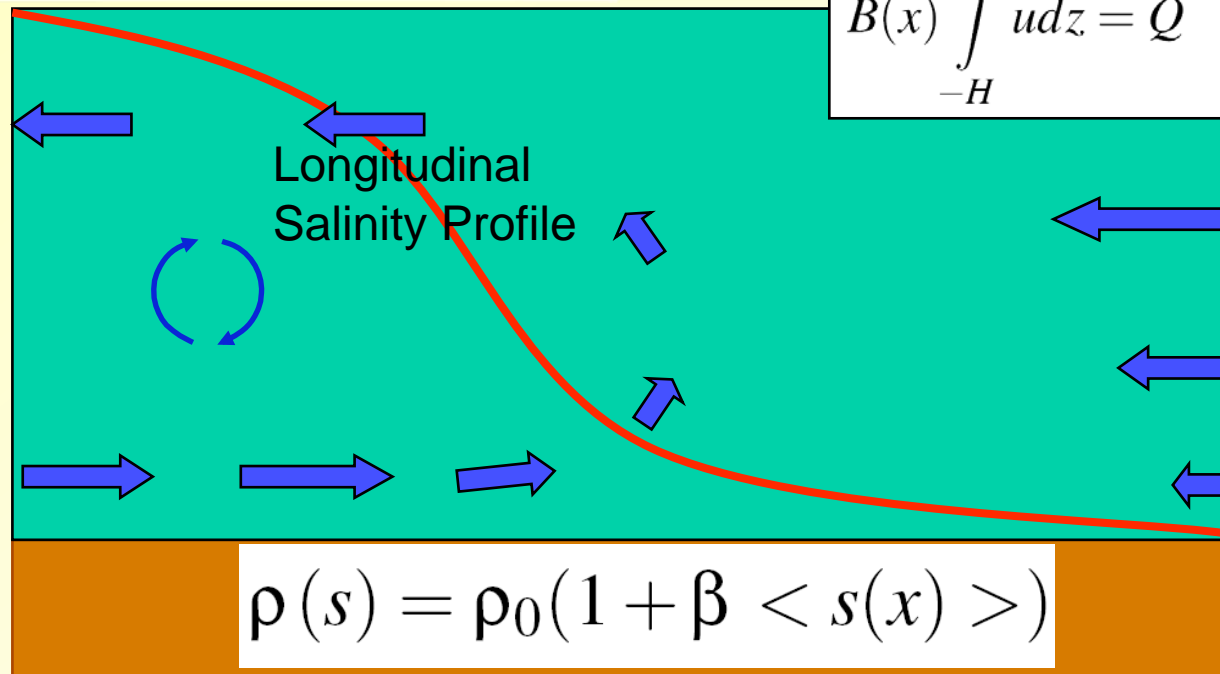
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+ appropriate boundary conditions

$$\zeta(t, x) = A_{M_2} \cos \sigma t + A_{M_4} \cos(2\sigma t - \phi)$$

$$B(x) \int_{-H}^{\zeta} u dz = Q \quad \text{at } x = L.$$



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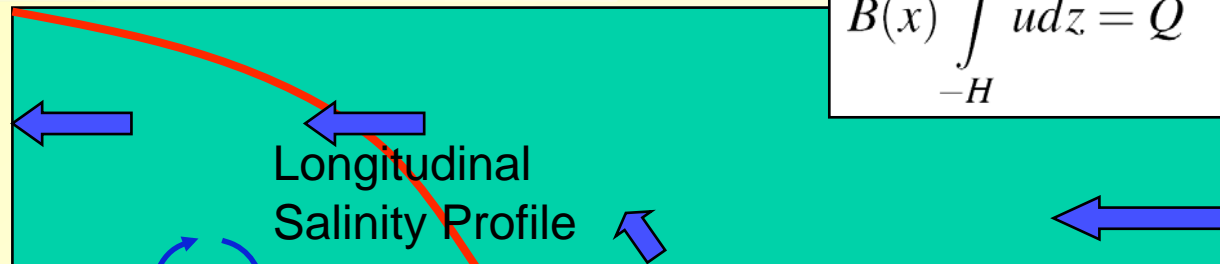
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In principle ρ depends on sediment concentration as well!

$$\rho(s) = \rho_0(1 + \beta \langle s(x) \rangle)$$

Model Formulation (3)

- Water Motion: 2 DV (width averaged) shallow water equations(residual, M_2 and M_4 components)
- Suspended load transport:
 - advection-diffusion equation
 - deposition
 - erosion $\sim a(x) |u|$

Erosion flux:
$$E_s \equiv -K_v \frac{\partial c}{\partial z} n_z - K_h \frac{\partial c}{\partial x} n_x = w_s c_*$$

Deposition flux:
$$D = w_s c n_z$$

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$$c_*(t, x) = \rho_s \frac{|\tau_b(t, x)|}{\rho_0 g' d_s} a(x)$$

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- Suspended load transport:
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 - deposition
 - erosion $\sim a(x) |u|$

- Diagnostic in density
- Bed evolution:

$$(1-p) \rho_s z_b = - \nabla \cdot \mathbf{q}_s$$



Convergence: increase of z_b Divergence: decrease of z_b

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$$(1-p) \delta_{\tau} z_b = - \nabla \cdot \mathbf{q}_s$$

With the flux $\mathbf{q}_s = \left\langle \int_H^{\zeta} (uc - K_h c_x) dz \right\rangle$

Solution Method (1)

Analytical solution method

Perturbation approach: physical variables are expanded in power series of a small parameter
 $\varepsilon = AM^2/H$.

Solution Method (2)


Analytical solution method



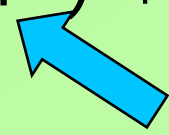
Velocities u and w
Concentration C

Shallow water equations

$$u = u^{02} + \varepsilon(u^{10} + u^{14}) + \dots$$

M_2 

 Residual


M_4 

 Internal

 External

Concentration equation

$$c = c^{00} + c^{04} + \dots + \varepsilon(c^{10} + c^{12} + \dots)$$

 Residual

 M_4

 Residual

 M_2

Residual M_4 Residual M_2

Solution Method (3)

Analytical solution method



Velocities u and w
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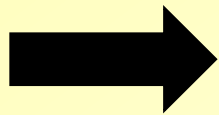
Residual sediment transport, that still depends on
the erosion coefficient $a(x)$

$$\int_{-H}^0 (u^{10} c^{00} + \langle u^{02} c^{12} \rangle + \langle u^{14} c^{04} \rangle - K_h \langle c_x^{00} \rangle) dz + \langle \zeta^0 [u^0 c^0]_{z=0} \rangle$$

Solution Method (4)

Residual sediment transport, that still depends on the erosion coefficient $a(x)$

- Assume morphodynamic equilibrium : no residual sediment transport



$$T(x) a(x) + F(x) a_x(x) = 0$$

- With $T(x)$:
- (red) $\sim \langle u \rangle \langle C \rangle$: residual contribution
 - (green) $\sim \langle u_{M_2} C_{M_2} \rangle$: settling lag (M_2)
 - (black) $\sim \langle u_{M_4} C_{M_4} \rangle$: tidal asymmetry (M_4)
 - (pink) diffusive contribution
 - (blue) sum of all terms
- $F(x)$:
- - (orange) $\sim \langle K_h C \rangle$: settling lag

Model Results (1)

Experiments

- Two years are considered: 1980 and 2005.
- Most parameters are obtained from observations

Model Results (1)

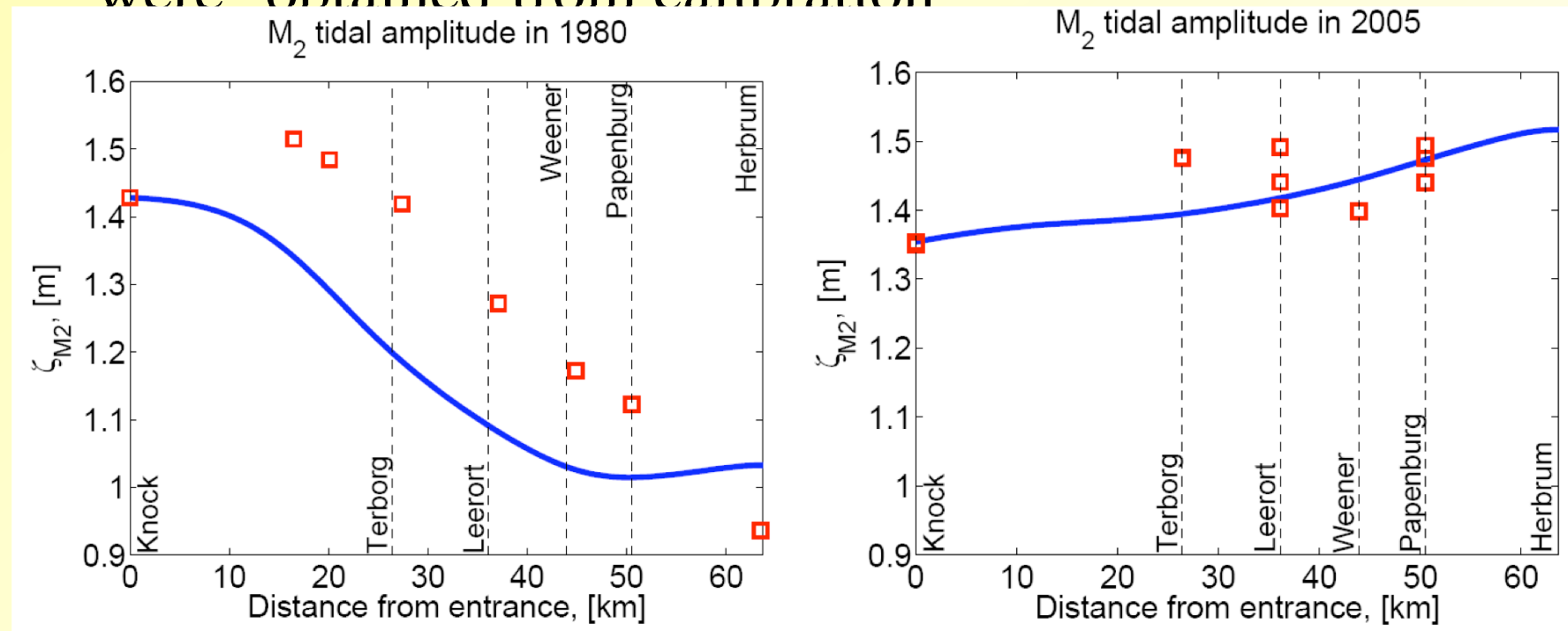
Experiments

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Model Results (2)

Experiments

- Two years are considered: 1980 and 2005.
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- Only the vertical mixing and bottom friction were obtained from calibration



0.0187 m^2/s
0.098 m/s

Vertical Mixing
Bottom Friction

0.0124 m^2/s
0.049 m/s

Model Results (3)

Experiments

- Two years are considered: 1980 and 2005.
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- Only the vertical mixing and bottom friction were obtained from calibration
- Furthermore we choose:
 - River outflow = $70 \text{ m}^3/\text{s}$
 - Settling velocity = 2 mm/s

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Using this information, we can solve for the unknown erosion coefficient:

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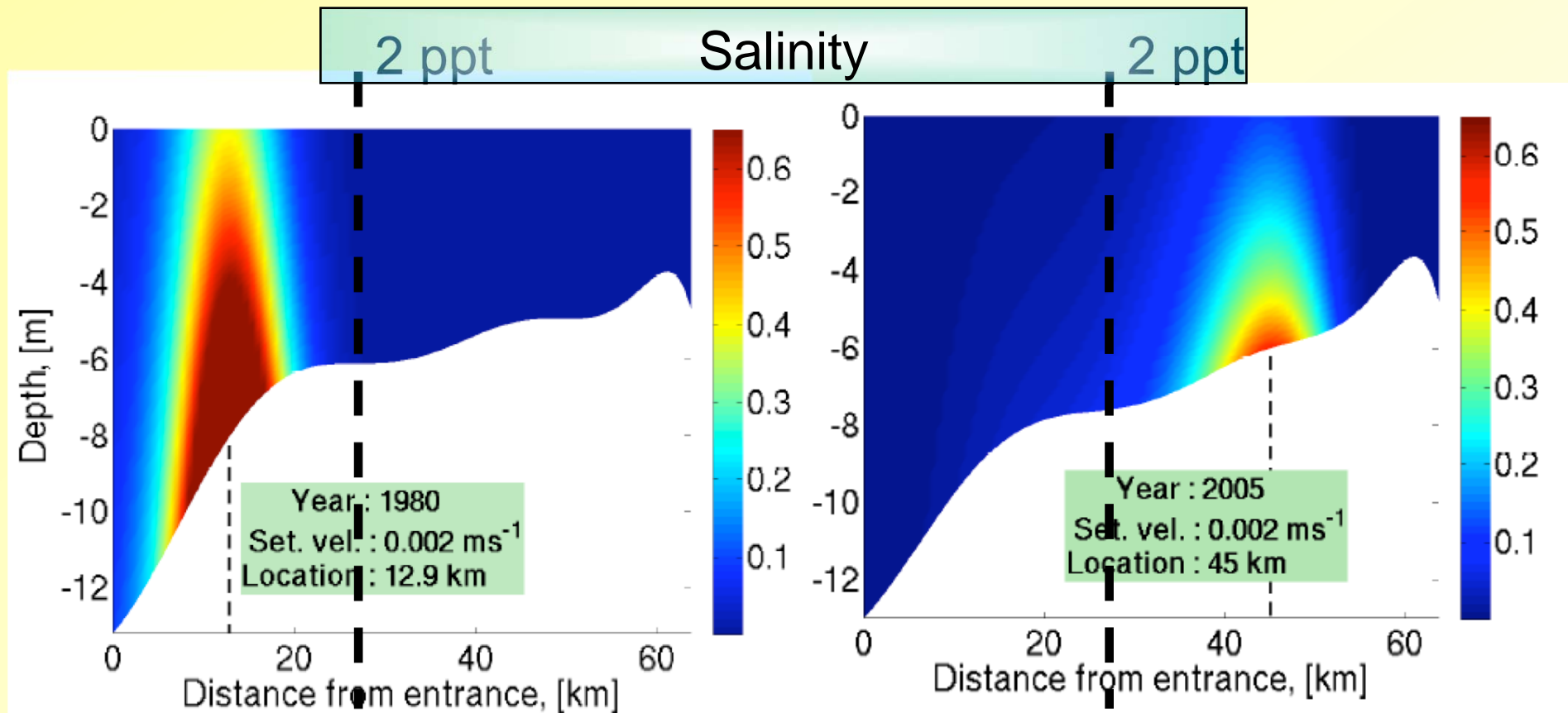
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This gives the sediment trapping in the estuary

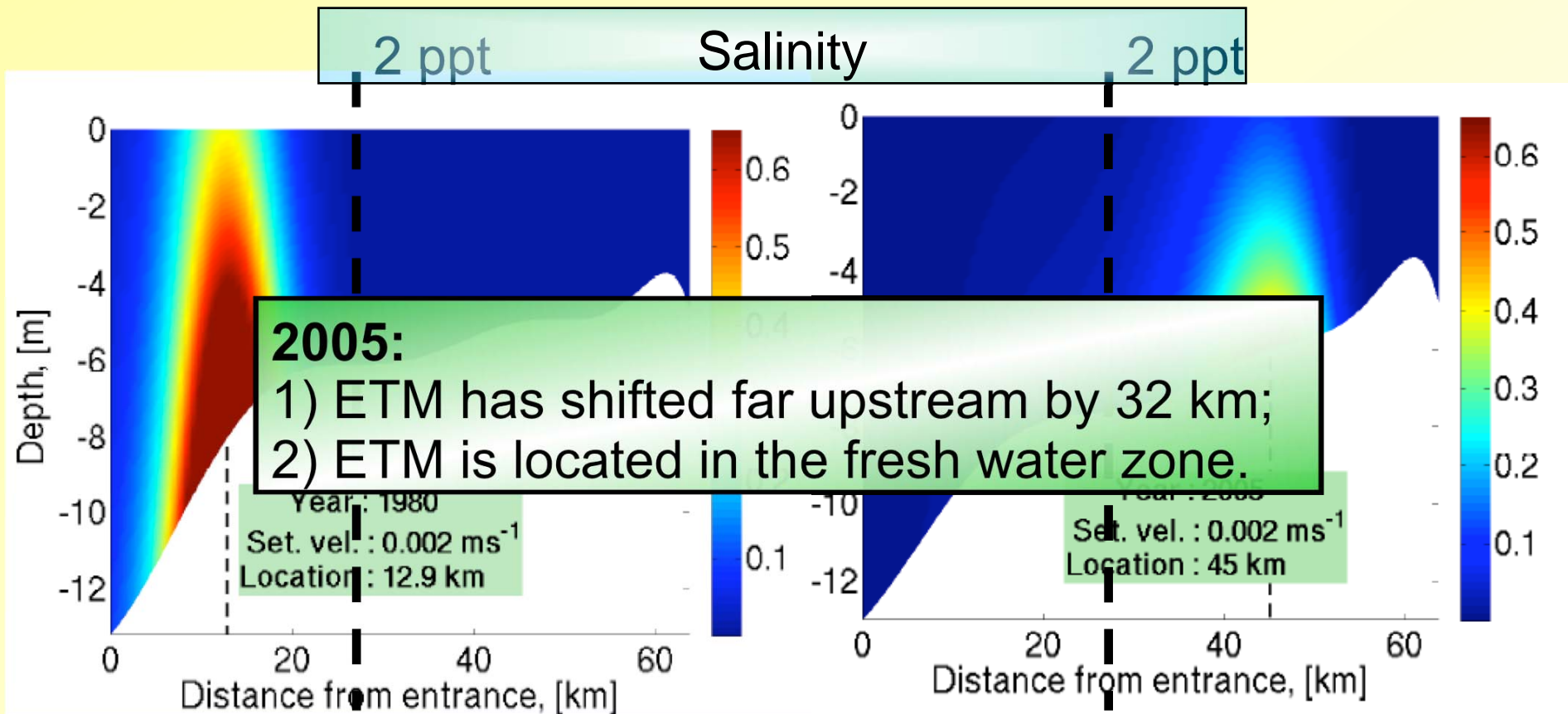
Model Results (5)



Model parameters:

- River discharge **$70 \text{ m}^3/\text{s}$** ;
- Setting velocity **2 mm/s** .

Model Results (5)



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Model Results (6)

Maximum of sediment concentration coincides with zeros of transport function T.

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So to understand the changes in the trapping location of the sediment, we have to inspect the function T and its different contributions more carefully:





Model Results (7)


$$T = \underbrace{\int_{-H}^0 u^{10} \frac{c^{00}}{a} dz + \left\langle \zeta \left[u^0 \frac{c^0}{a} \right]_{z=0} \right\rangle}_{T_{res}} + \underbrace{\int_{-H}^0 \left\langle u^{02} \frac{c^{12}}{a} \right\rangle dz}_{T_{M_2}} + \underbrace{\int_{-H}^0 \left\langle u^{14} \frac{c^{04}}{a} \right\rangle dz}_{T_{M_4}} - \underbrace{\int_{-H}^0 K_h \left\langle \frac{c^{00}}{a} \right\rangle_x dz}_{T_{diff}}.$$

Components of the transport function T:

 $\int_{-H}^0 u^{10} c^{00} dz + \langle \zeta [u^0 c^0]_{z=0} \rangle$ Residual transport function

 $\int_{-H}^0 \langle u^{02} c^{12} \rangle dz$ M_2 transport function


 $\int_{-H}^0 \langle u^{14} c^{04} \rangle dz$ M_4 transport function

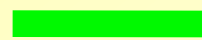
 $\int_{-H}^0 K_h \langle c_x^{00} \rangle dz$ Diff. transport func.


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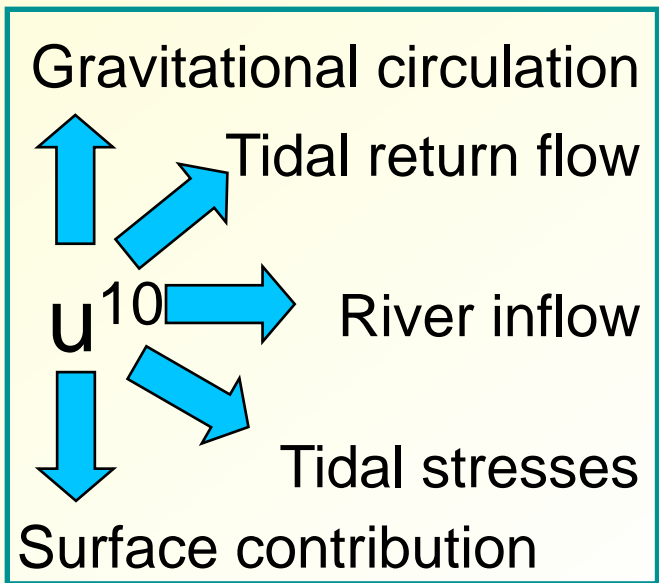
Components of the transport function T:

 $\int_{-H}^0 u^{10} c^{00} dz + \langle \zeta [u^0 c^0]_{z=0} \rangle$ Residual transport function

 $\int_{-H}^0 \langle u^{02} c^{12} \rangle dz$ M₂ transport function

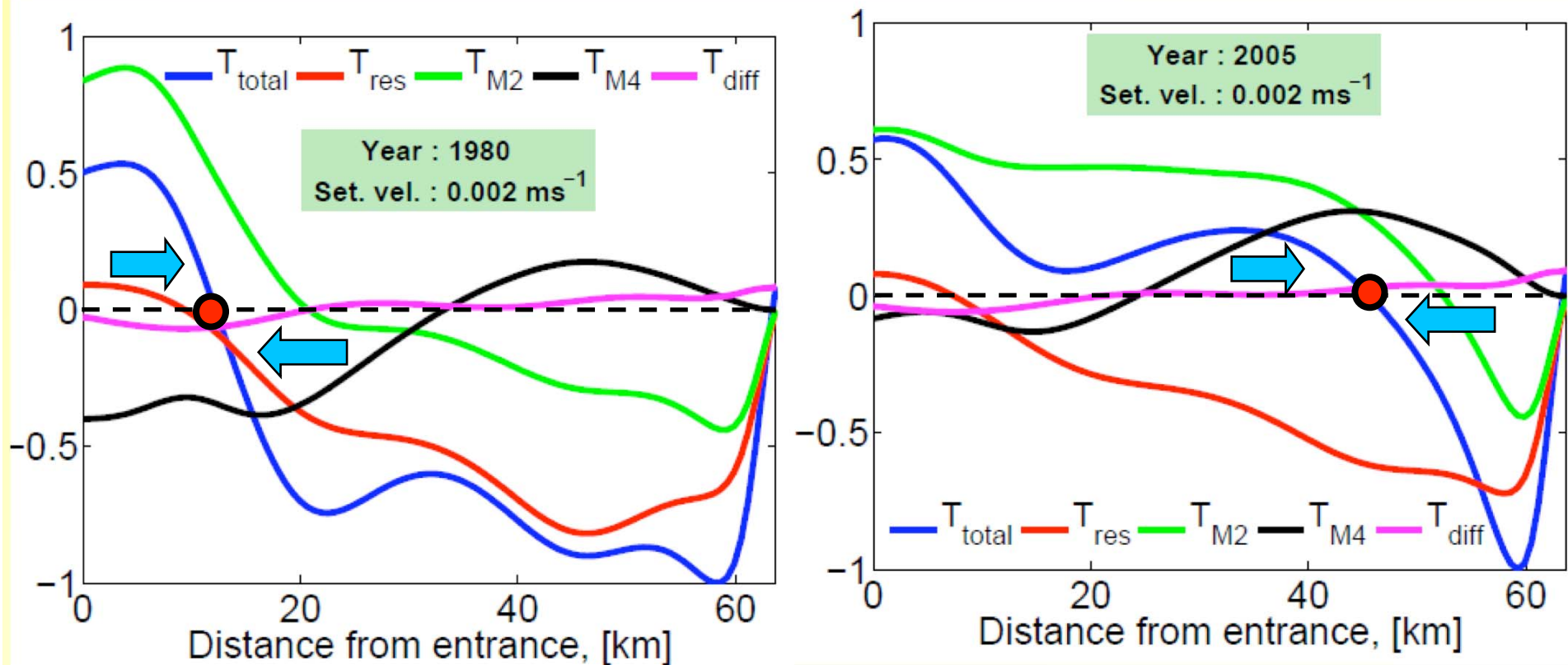
 $\int_{-H}^0 \langle u^{14} c^{04} \rangle dz$ M₄ transport function

 $\int_{-H}^0 K_h \langle c_x^{00} \rangle dz$ Diff. transport func.



Model Results (7)

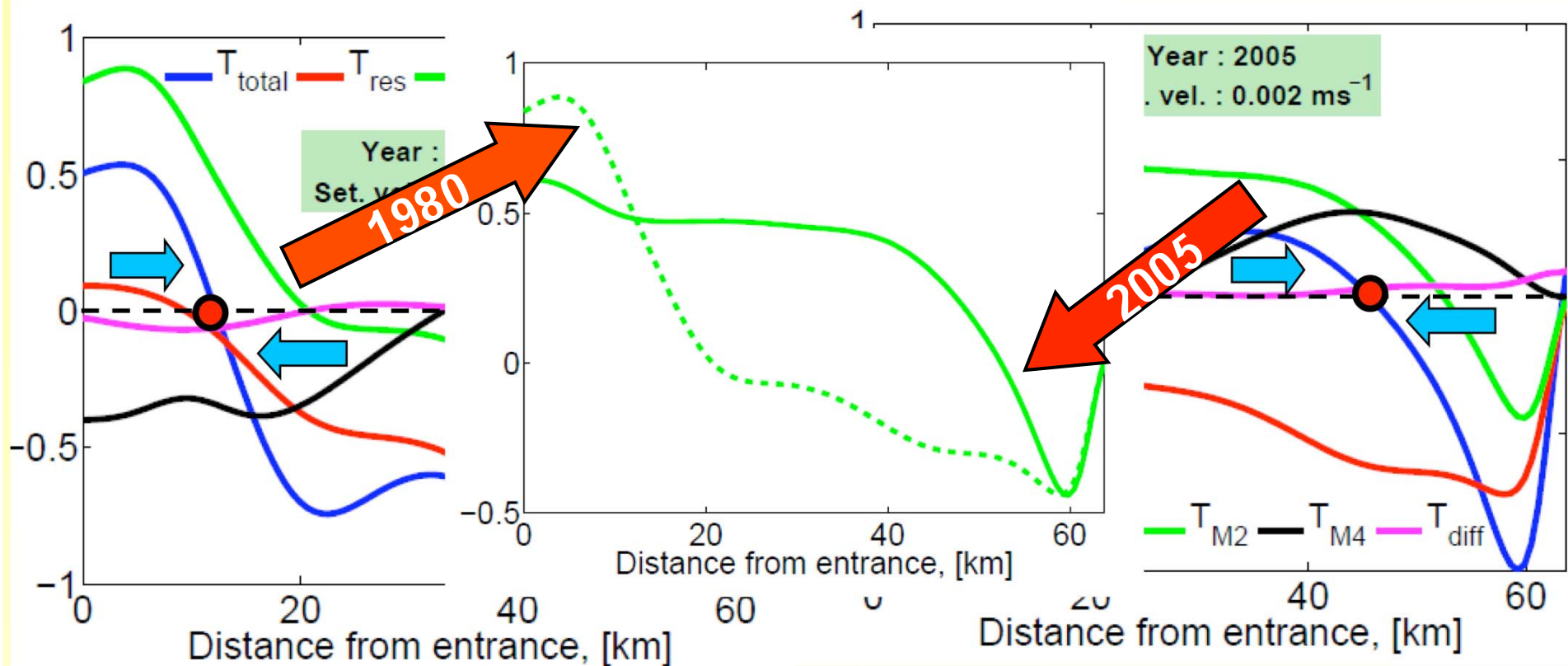
Maximum of sediment concentration coincides with zeros of transport function T .



The convergence point has moved upstream mainly due to change of the M_2 contribution

Model Results (7)

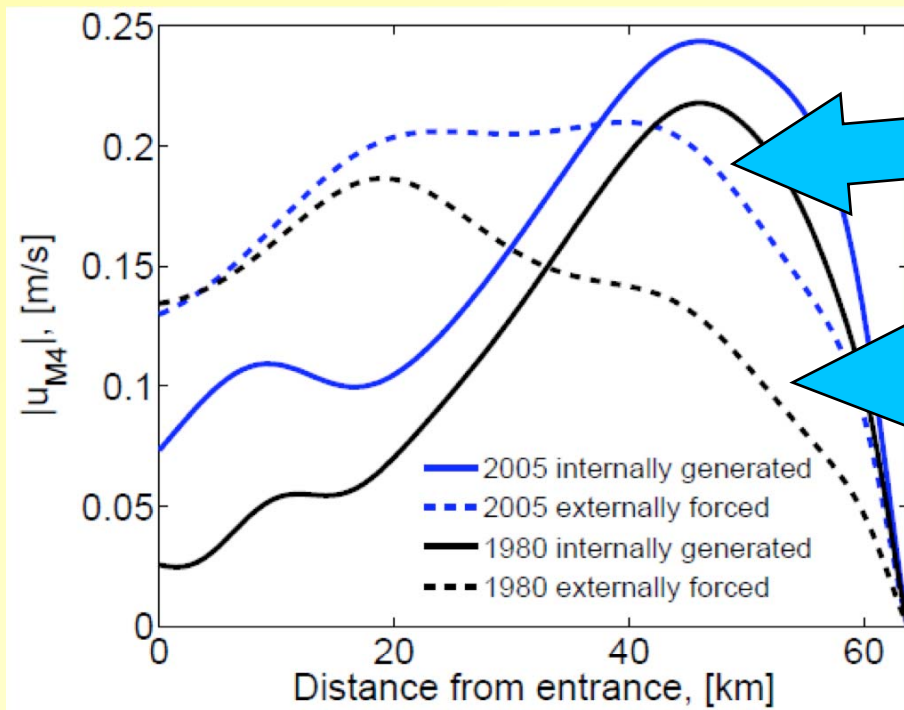
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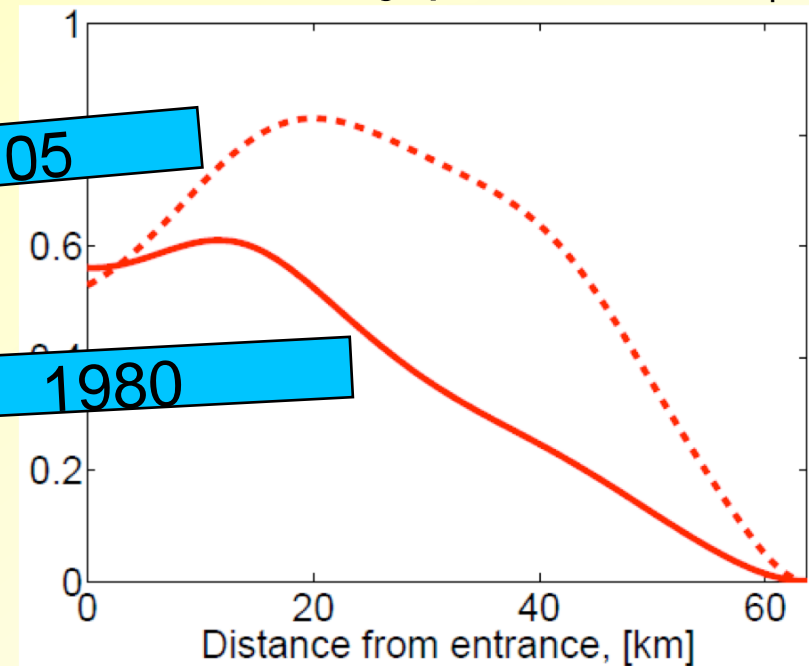
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Model Results (8)

M_4 velocity amplitude



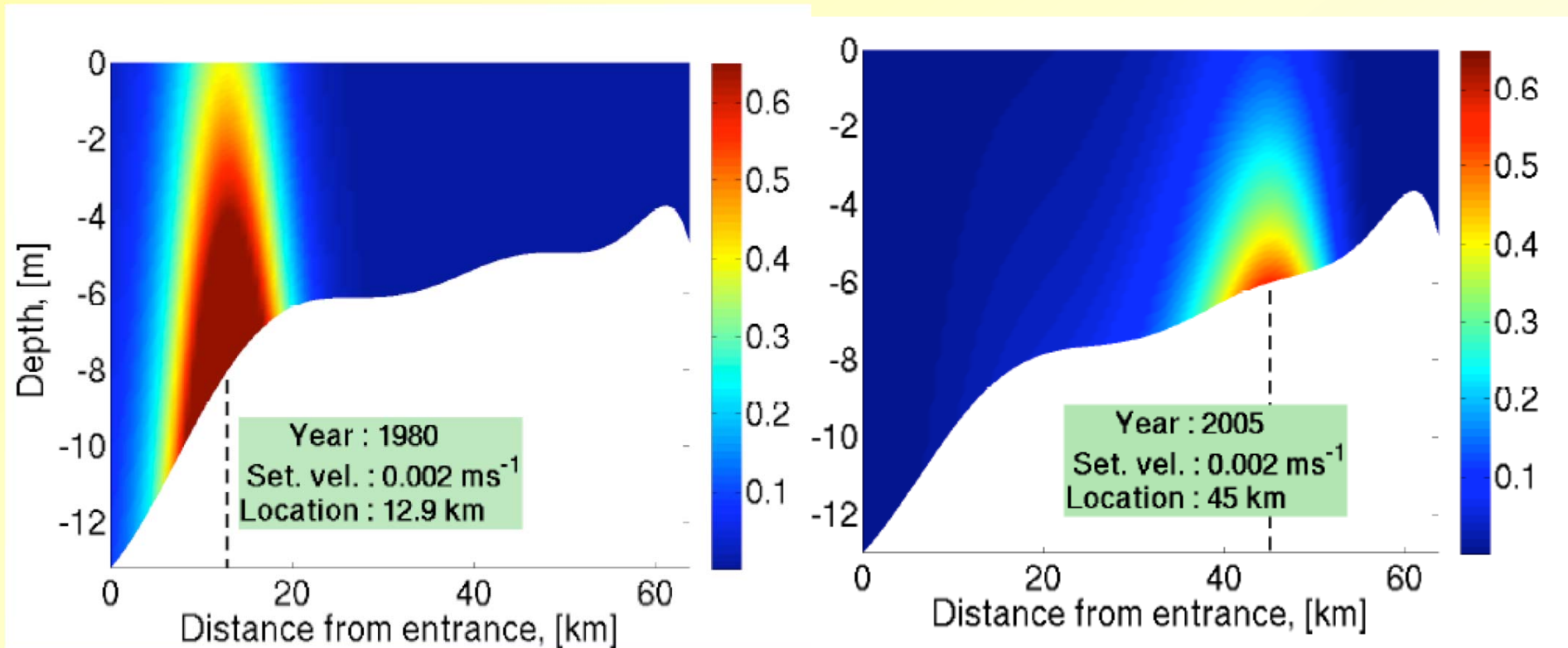
Contribution of T_{M_2} due to externally prescribed M_4



The behavior of the T_{M_2} component has changed due to changes in the externally prescribed M_4 :

TIDAL ASYMMETRY MECHANISM

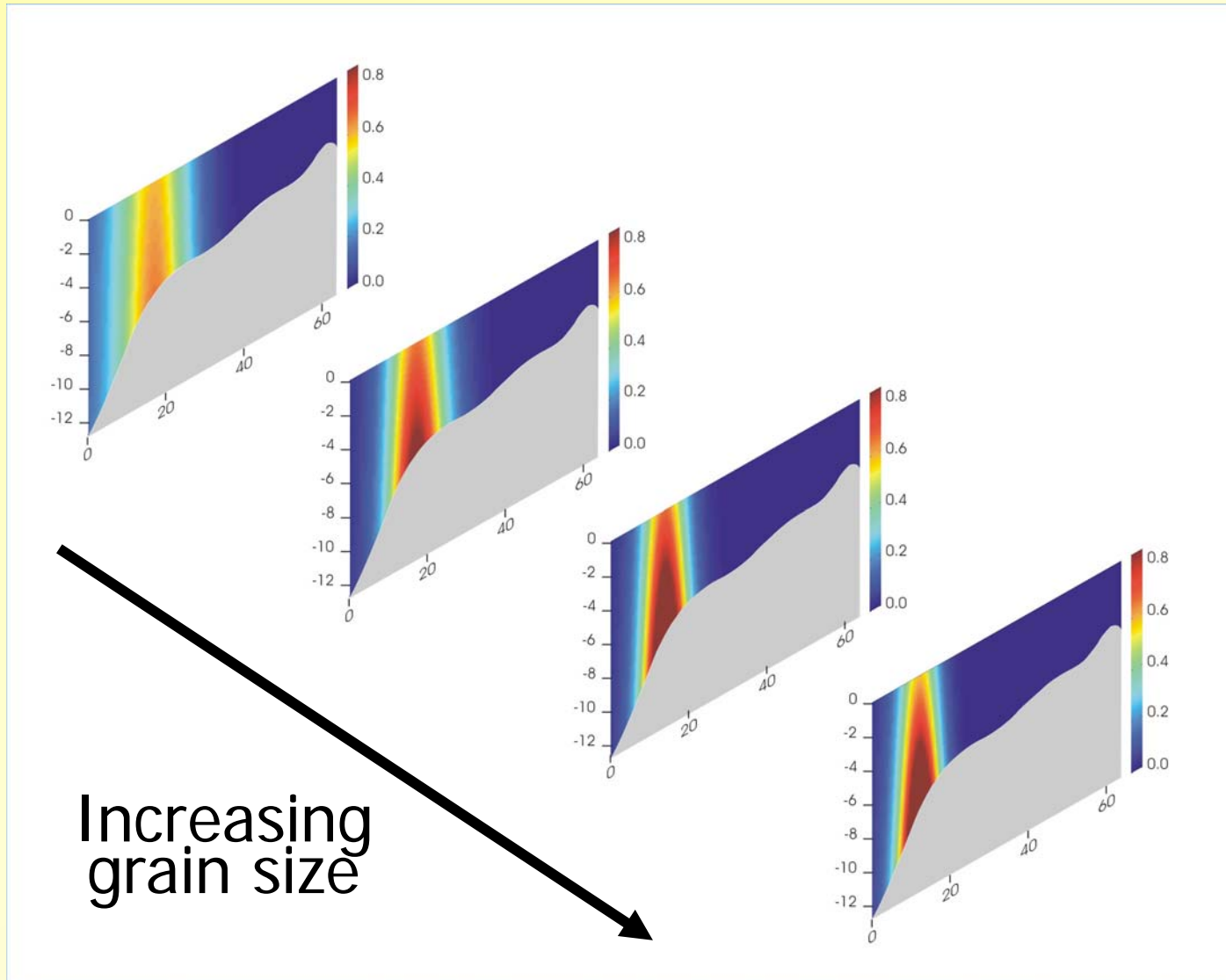
Model Results (9)



**CHANGE OF TRAPPING LOCATION DUE TO
CHANGE IN TIDAL ASYMMETRY
(CHARACTER OF M4 TIDAL WAVE)**

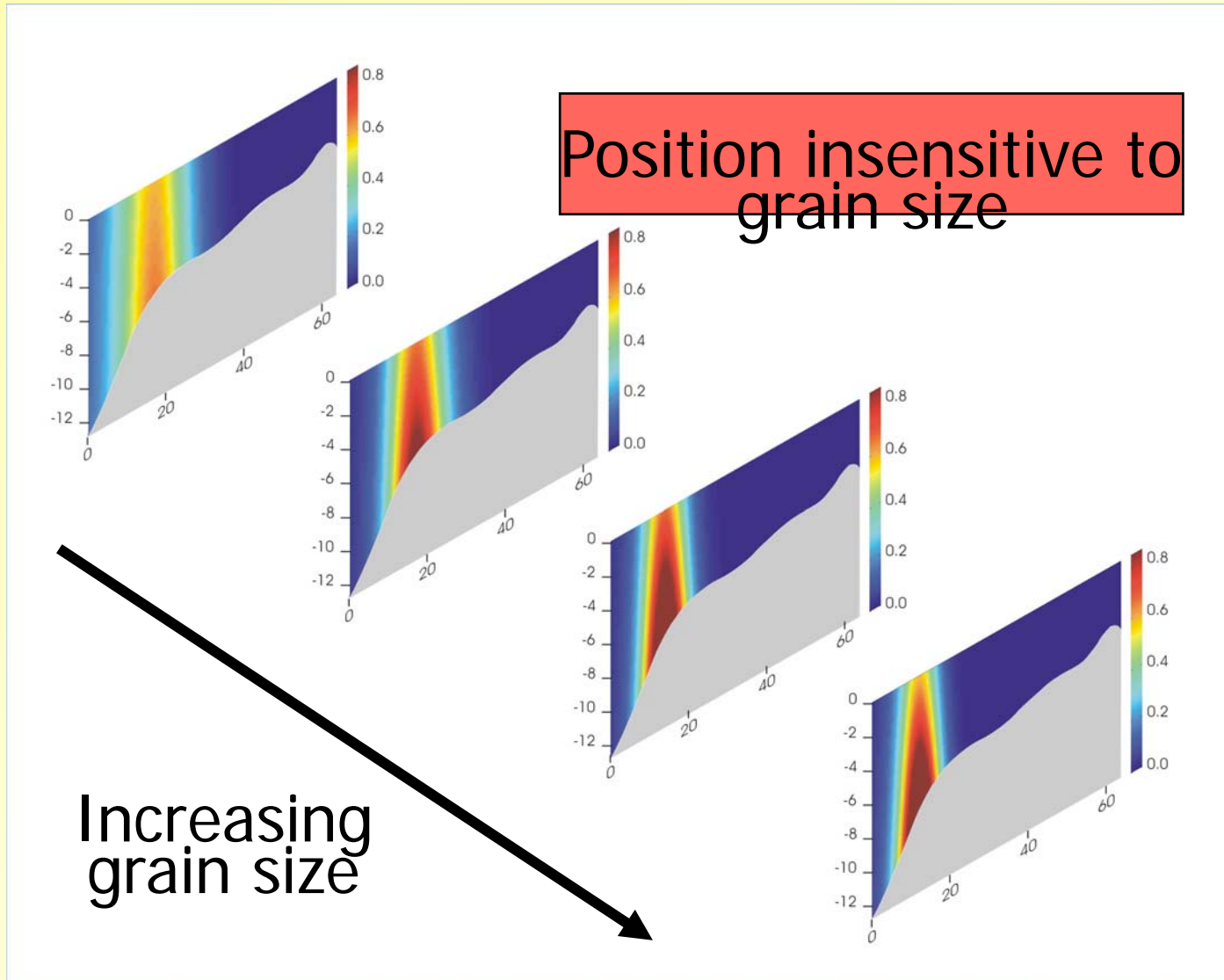
Model Results (10)

Dependency on grain size (1980)



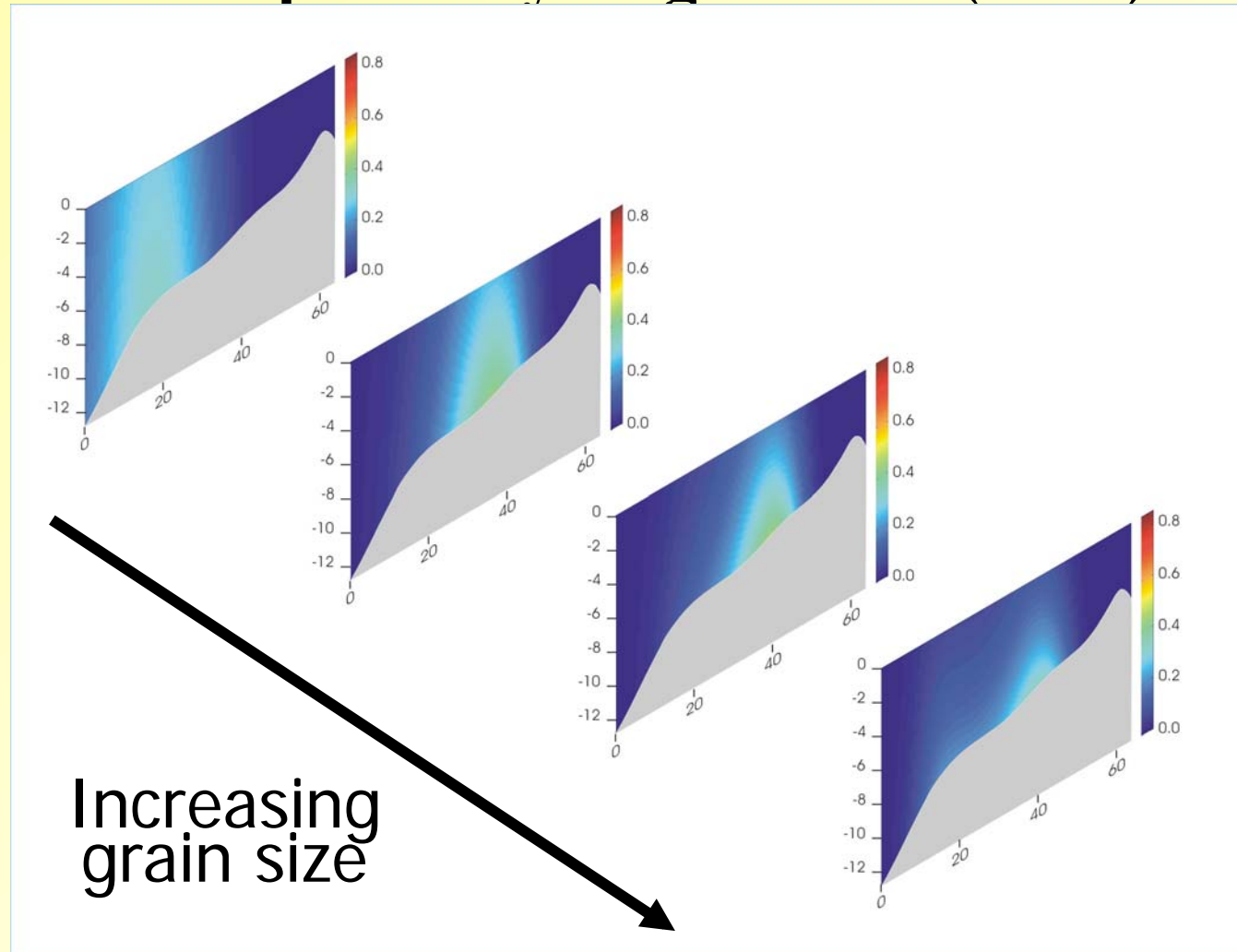
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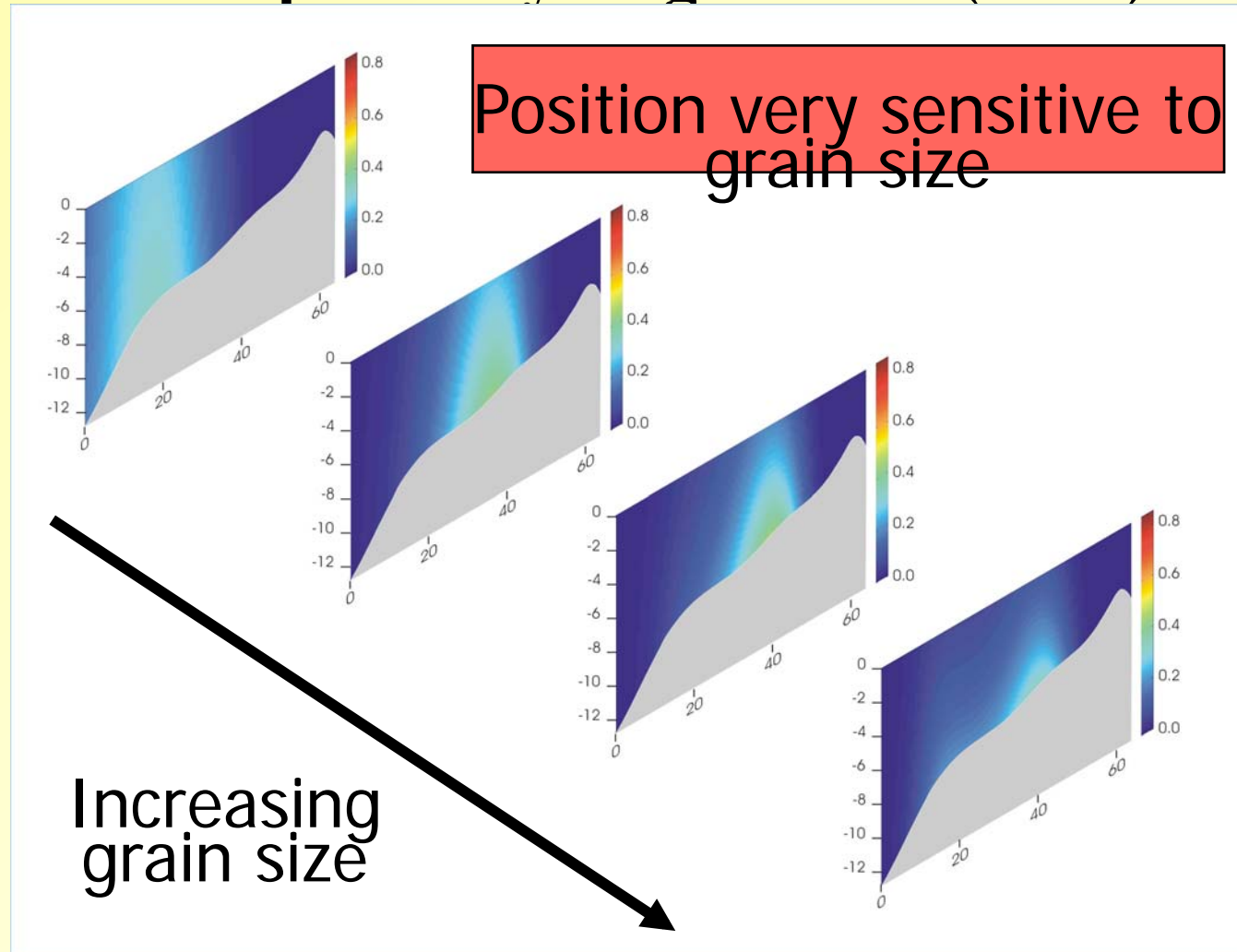
Model Results (11)

Dependency on grain size (2005)



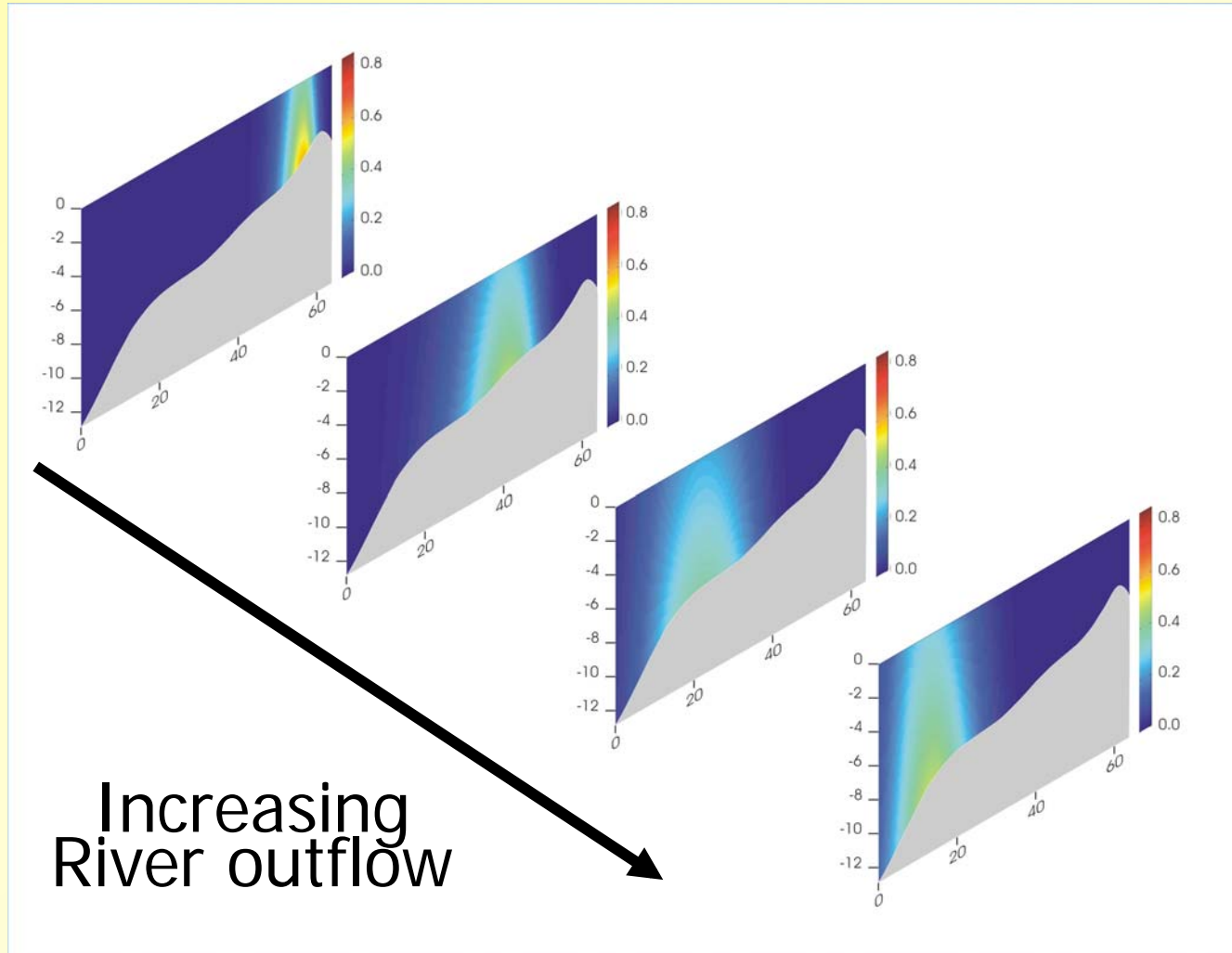
Model Results (11)

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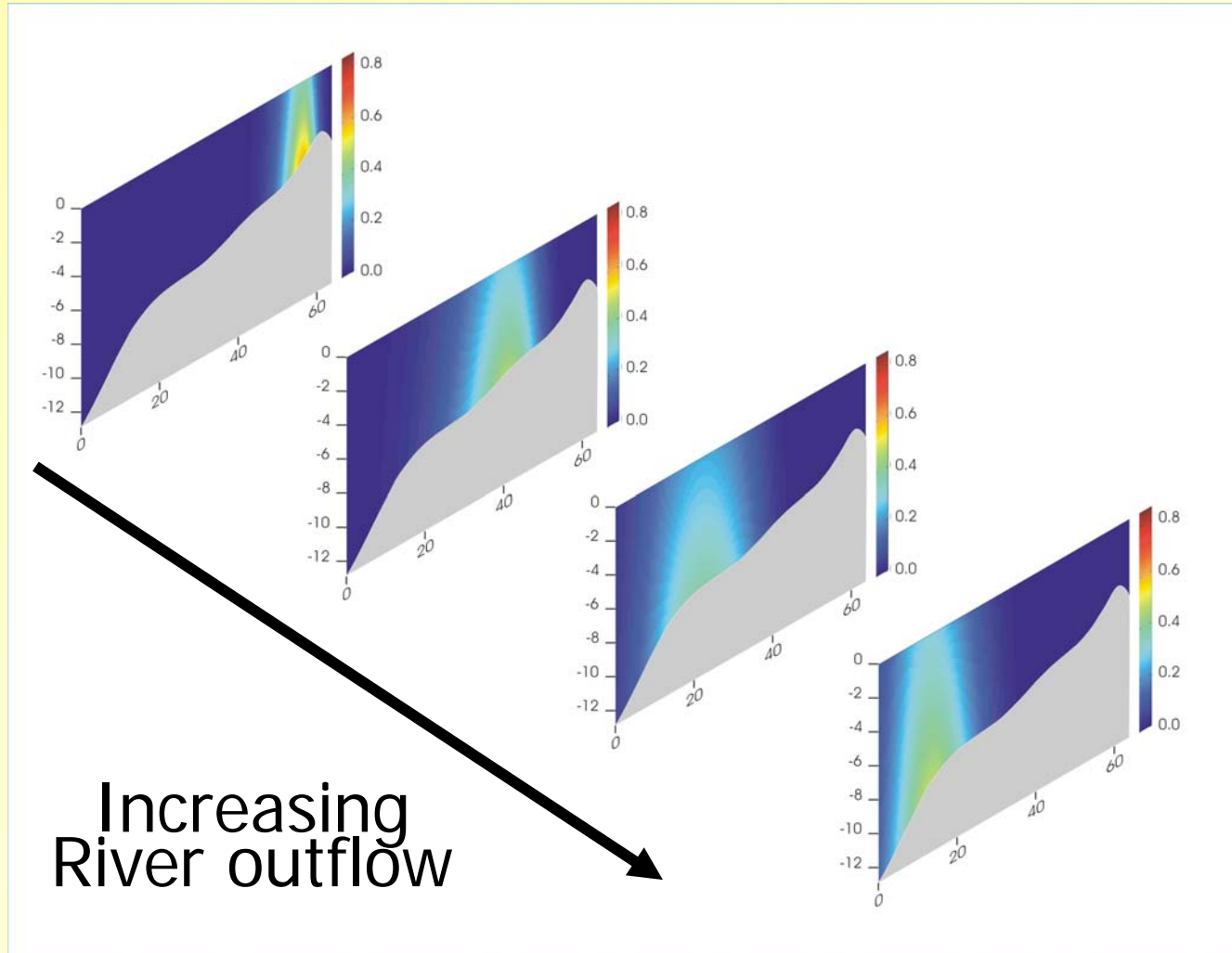
Model Results (12)

Dependency on river outflow (2005)



Model Results (13)

Dependency on river outflow (2005)



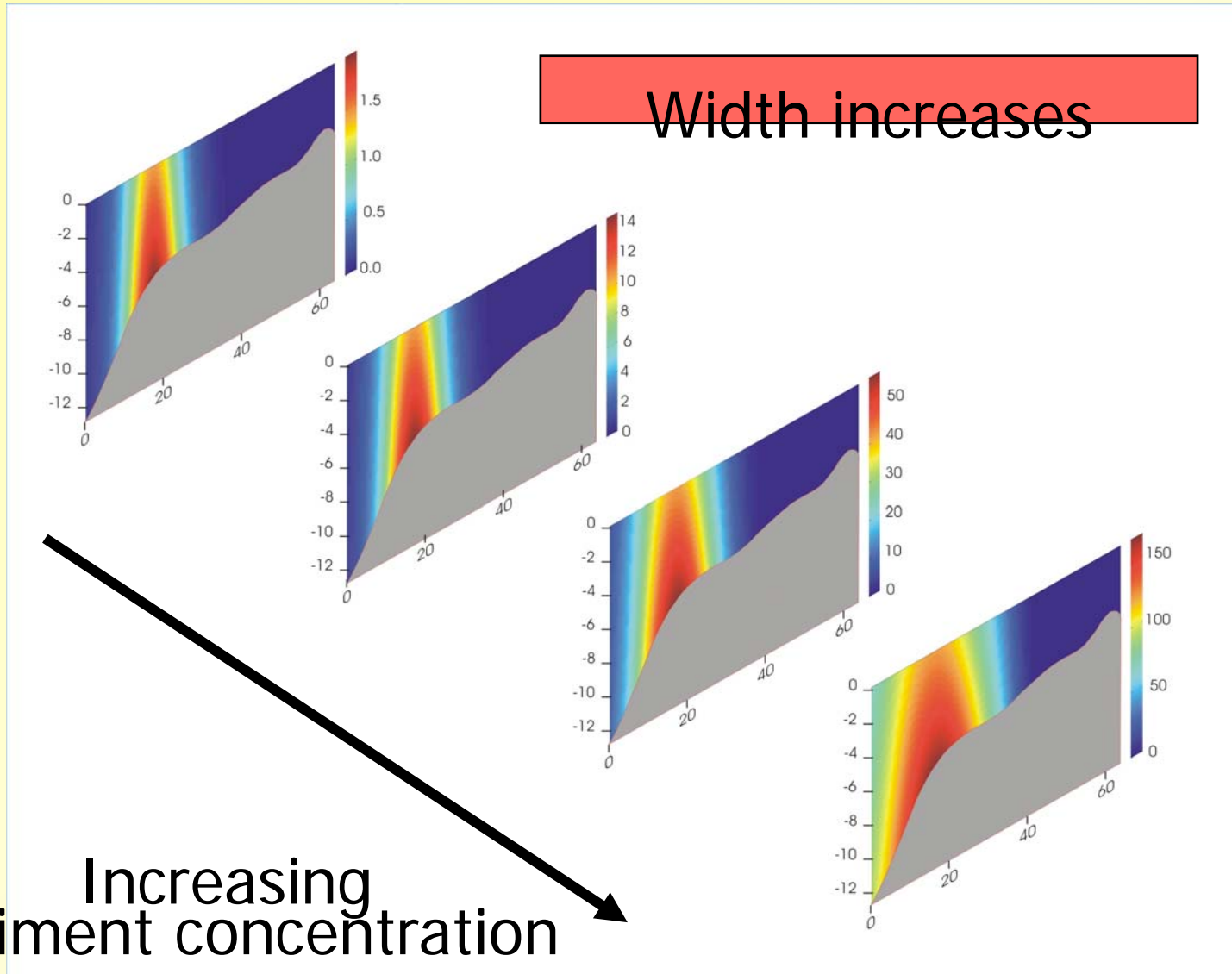
Model Results (14)

Extending the model by making density depend on
Sediment concentration as well

Results in a nonlinear differential equation for
the sediment availability $a(x)$

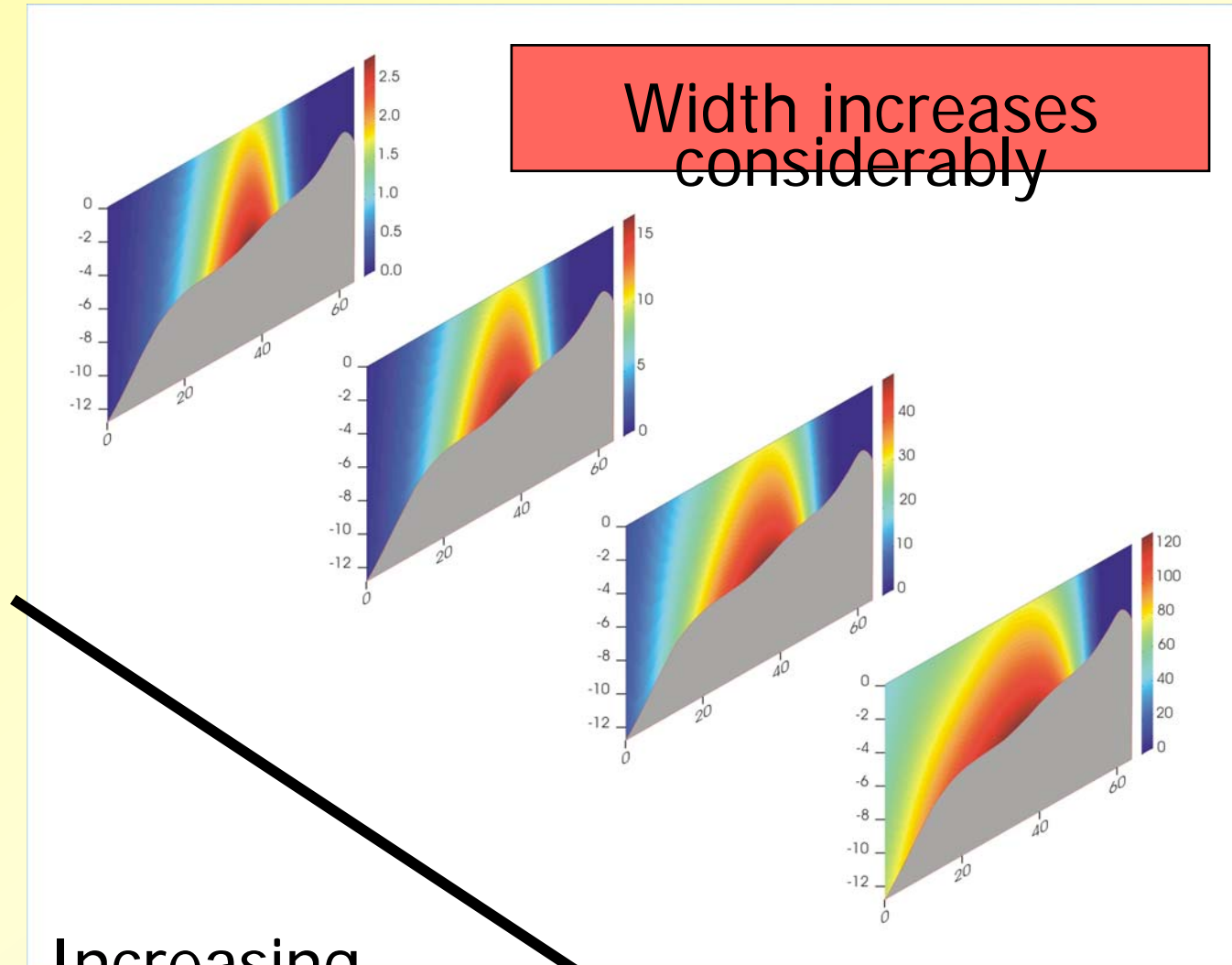
Model Results (15)

Results for the 1980 case



Model Results (16)

Results for the 2005 case



Width increases considerably

Increasing Sediment concentration

Conclusions

- Formation of ETMs can be modelled with an idealised model. Essential Ingredients:
 - Along-estuary **varying** erosion coefficient (~ layer of fine sediment)
 - **Tidal asymmetry**
- Physical mechanisms resulting in the ETMs can be understood using the idealised model.
- Difference in trapping of sediment in Ems Estuary mainly a result of the changes in tidal asymmetry between 1980 and 2005.
- Model sensitivities to parameters and parameterizations can be easily investigated. The trapping locations in 1980 are not very sensitive to parameter changes, in 2005 the locations change dramatically when changing parameters.